

## COMPARATIVE STUDY ON STATIC AND DYNAMIC ANALYSIS OF STRUCTURES

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### Abstract: -

As the modern buildings have been gotten taller and narrower than before, the structural engineers have to perform both static and dynamic analysis for seismic loads that may affect on structures in order to make sure of the safety verifications and the optimal design requirements. The two common methods that always used for structural analysis against lateral loads are equivalent static method and response spectrum analysis. However, some different limits and restrictions for using the first method are stated by the universal design codes. This research studies the differences between the two methods through the results of seismic analysis by using Egyptian code of practice 2012, European Code 8: 2004 and Uniform Building Code 1997. It has been concluded that the equivalent static analysis method always gives higher results for drifts and overturning moments than those of response spectrum analysis method in case of using the aforementioned three design codes.

**Keywords:** - Seismic analysis, response spectrum method, equivalent static method

في العصر الحديث زادت ارتفاعات المباني واصبحت اكثر نحافة عما قبل ولذلك يجب على المصمم الانشائي اجراء كل من التحليل الاستاتيكي والديناميكي للمباني تحت تأثير الاحمال الافقية وذلك لتحقيق متطلبات الامان والوصول الى درجة الامثلية من التحليل الانشائي. هناك طريقتين اكثر شيوعا واستخداما في التحليل الزلزالي للمباني العالية وهما طريقة الحمل الاستاتيكي المكافئ وطريقة طيف التجاوب. ولكن هناك قيود تم ذكرها في بعض الكودات العالمية تحكم استخدام الطريقة الاولى ولذلك ركز هذا البحث على مقارنة نتائج كلتا الطريقتين السابقتين من التحليل الزلزالي على برنامج الايتابس باستخدام مجموعة من الكودات وهي الكود المصري والكود الاوروبي والكود الامريكى وتم استنتاج ان طريقة الحمل الاستاتيكي المكافئ دائما تعطى نتائج اعلى من طريقة طيف التجاوب الافقى المرن من حيث نتائج الازاحة الافقية ونتائج عزوم الانقلاب في حالة استخدام الاكواد الثلاثة.

### Introduction:-

Seismic design of tall buildings is primarily concerned with structural safety during major earthquake; however, serviceability, human comfort and the potential for economic loss are also of concern. Seismic analysis requires an understanding of the structural performance under large inelastic deformations. Biswas, R. [4] demonstrated the accuracy and the exactness of equivalent static analysis in comparison with the most commonly adopted method, response spectrum analysis. Mahmoud, S., and Abdallah, W., [5], evaluated the seismic performance of an existing shear wall residential building located in Cairo using response spectrum analysis and equivalent static force methods in the seismic analysis. Srikanth, B., and Ramesh, V., [6] also compared the two different methods according IS code. Then, they concluded that there are a significant differences in building's responses obtained using the two methods. Bagheri, B., et al, [7] compared the results of drift at top for 20-storey RC building, which obtained from equivalent static method, response spectrum method and time history method by using elcentro earthquake 1940. The main objective of this paper is to study the limitations of using equivalent static method in case of Egyptian Code of Practice, ECP 2012 [1], European Code 8: 2004, EC8: 2004 [2], and Uniform Building Code, UBC1997[3].

### Research methodology:-

In the present study, regular shear wall buildings with seven different level of heights, started by 5 stories and gradually increased to pass 10, 14, 17, 20, 24 and 30 stories with the same plane are modeled using software packages ETABS. Each case is analyzed for the same lateral loads using the two different analysis methods, the static and dynamic analysis methods. Both of the two methods are based on elastic response spectrum curve using ECP 2012, EC8: 2004 and UBC 1997. For the aim of comparison, the results of displacements at top and the differences between the results of the two methods are tabulated versus each case. Based on the differences between the results of the two methods, the limitations of using linear static analysis method in seismic analysis can be concluded for each design code.

### Building Description:-

The structural system that adopted for the studied cases is shear wall system with central core and four shear walls in x-direction and six shear walls y-direction whereas the adopted schematic plane for this study is shown in Fig. (1).

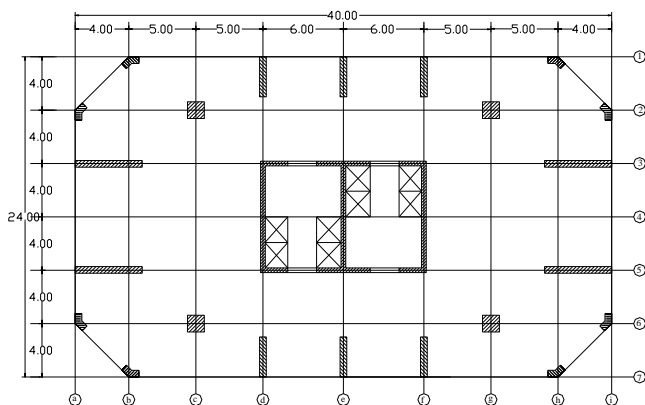


Figure (1): Schematic plane for shear wall system

This plane is repeated for all floors in all buildings without any changes or setbacks. The seven levels of heights for the shear wall system are shown in Fig. (2).

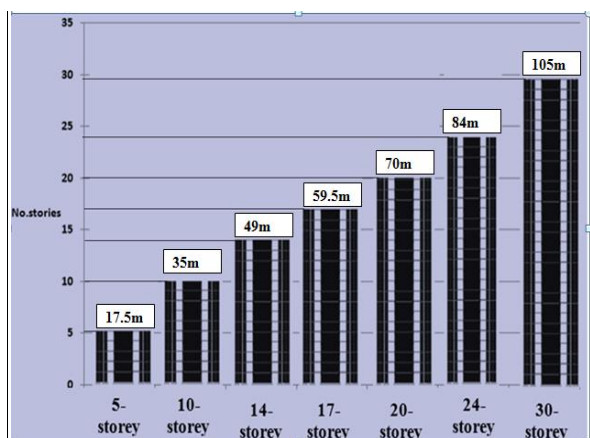


Figure (2): The studied buildings

The cross sectional areas for both columns and shear walls are designed against the determined ultimate gravity loads at the base for each building by using the ultimate load equation that stated in ECP 2012, [1], as the following

$$P_{ult} = 0.35f_{cu}A_c + 0.67f_yA_s \quad \text{Eq. (1)}$$

Where

- $P_{ult}$  Ultimate load calculated at base
- $A_c$  Area of concrete for section under study
- $f_{cu}$  Ultimate compressive strength for concrete
- $A_s$  Area steel in cross section
- $F_y$  Yield stress for the reinforced bars

### General Assumption for Primary Design of Vertical Elements:-

- 1) The ultimate load,  $P_{ult}$  is calculated for each vertical member by aggregating the supposed gravity loads above the foundation level based on the load combination,  $P_{ult} = 1.4DL + 1.6LL$

- 2) This pattern is applied for each system separately
- 3) Floor thickness,  $t_s$  is considered 25cm for all buildings
- 4) Concrete cover for all vertical elements is assumed 4.0cm
- 5) Compressive strength for concrete,  $f_{cu}$  is assumed 350kg/cm<sup>2</sup> for all concrete elements
- 6) Live load is assumed 300kg/m<sup>2</sup> uniformly distributed over the entire floor area
- 7) Total uniform dead load is assumed equal (flooring cover 150kg/m<sup>2</sup> + walls and partitions 400kg/m<sup>2</sup> = 550kg/m<sup>2</sup>)
- 8) Thickness of core wall is considered 20, 25, 27, 29, 31, 33 and 35 cm for the 5, 10, 14, 17, 20, 24, and 30-storey buildings respectively
- 9) For each building the cross sectional area for vertical elements is considered constant through the entire height of the building
- 10) Yield strength for high tensile steel,  $f_y$  is considered 3600kg/cm<sup>2</sup> and the area of steel inside the section is allowed to equal 0.2% of area concrete for compression members

Substituting with the previous assumptions in the ultimate load formula Eq. (1), the area concrete of the any section can be given as a function of load as the following:

$$P_{ult} = 170.74A_c \quad \text{Eq. (2)}$$

### Methods of Analyses:-

The adopted methods for seismic analysis are equivalent static method and response spectrum method

### Equivalent Static Method:-

Seismic analysis by this method is considered sufficient for regular, low to medium-rise buildings. This is permitted in most codes of practice. It begins with an estimation of base shear load and its distribution on each story calculated by using formulas given in the considered codes, [1-3]. However, for high-rise buildings where second and higher modes can be important, or buildings with torsional effects, the implementation of equivalent static method is considered not sufficient and complex methods such as response spectrum method and time history method are required used in these circumstances.

The specified Seismic Parameters for Equivalent Static Method are summarized for each code as given in Table (1)

**Table (1):** Parameters of equivalent static method

code	Considered seismic parameters
ECP 2012 & EC8: 2004	<ul style="list-style-type: none"> <li>• Response spectrum type (1)</li> <li>• Soil class (B)</li> <li>• TB, TC and TD are 0.05, 0.25 and 1.2 respectively</li> <li>• Response modification factor, R = 4.5, 4 for ECP 2012, EC8: 2004 respectively</li> <li>• Ground acceleration, <math>a_g = 0.125g</math> and <math>0.15g</math> for ECP 2012, EC8: 2004 respectively</li> <li>• Correction factor, <math>\eta = 1</math></li> <li>• Importance factor, <math>\gamma = 1</math></li> <li>• Time period, <math>T = 0.05H^{0.75}</math></li> </ul>
UBC 1997	<ul style="list-style-type: none"> <li>• Seismic zone (2A) with seismic zone factor, 0.15</li> <li>• Soil profile (<math>S_C</math>)</li> <li>• Seismic coefficients, <math>C_a = 0.18</math>, <math>C_v = 0.25</math></li> <li>• Time period, <math>T = CtH^{0.75}</math>, (<math>Ct = 0.035</math>)</li> <li>• Over strength factor, R = 4.5</li> <li>• Importance factor, <math>\gamma = 1</math></li> </ul>

**Response Spectrum Method:-**

A plot of maximum dynamic response, such as accelerations versus the natural periods of the building gives us an acceleration response spectrum. This curve is determined in accordance with the site conditions such as soil profile, damping factor and return period of maximum capable earthquake.

**What ETABS does?**

Is that, it calculates the maximum acceleration versus the natural period of structure then, the maximum acceleration is incorporated with seismic weight and other seismic parameters that have been defined to the program according to a certain code. By performing the analysis, the base shear is determined, distributed through the height and affect horizontally tried to bend the structure over the ground.

The specified elastic response spectrum curve that adopted for response spectrum analysis versus each code are summarized in Table (2), whereas the seismic parameters in Table (1) are taken in mind.

**Table (2):** Specified Response Spectrum Curves

code	Elastic response spectrum curve
ECP 2012	
EC8: 2004	
UBC 1997	

To convert these curves from elastic state to the design state, a correction factor equal  $(9.81/R)$  is multiplied by their case of loading.

**General Assumptions for Modeling and Analysis:-**

- 1) Orientations and spans for vertical elements are considered constant through the height
- 2) Service core area is considered the same for all cases
- 3) The beam that connects the core walls, is considered  $35 \times 100cm$  through the entire height of the building
- 4) Story height is considered 3.50 m for all cases
- 5) Hall and service core area are connected with horizontal rigid diaphragms
- 6) Service core area is defined as a pier section in ETABS

- 7) All cases are considered rested on fixed foundation
- 8) Material specifications for reinforced concrete are the same for all cases
- 9) The applied lateral loads are represented only in seismic loads
- 10) The assigned mass source to the program in order to measure the seismic weight is commonly used as a combination of total dead loads plus 50% of live loads
- 11) Constant percents from the full inertia for all vertical and horizontal elements are assumed to participate in seismic resistance in order to take the effects of cracking into consideration

**Analysis and Results: -**

The seven cases have been modeled and analyzed using the two considered methods then the results of both displacements at top and overturning moments at base are obtained and tabulated versus each case and code

**a. Results of Displacement at Top**

Tables (3, 4 and 5) give the results of displacements at top versus each case for ECP 1212, EC8: 2004 and UBC 1997 respectively

**Table (3):** Drift values for both static and dynamic analysis by ECP 2012

Buildings	Static analysis	Dynamic analysis	Difference ratio%
5-storey	0.70	0.60	21.00
10-storey	2.01	1.58	21.39
14-storey	4.03	3.12	22.58
17-storey	6.87	5.21	24.16
20-storey	10.8	8.07	25.28
24-storey	15.2	11.3	25.66
30-storey	34.9	25.3	27.51

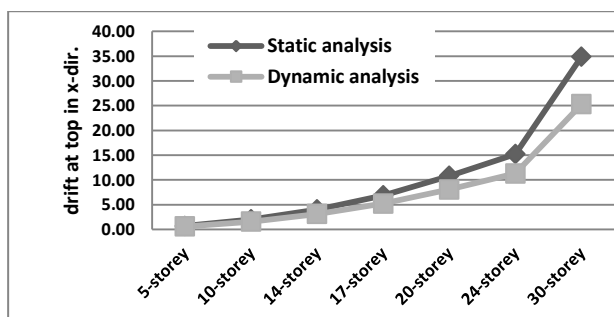
**Table (4):** Drift values for both static and dynamic analysis by EC8:2004

Buildings	Static analysis	Dynamic analysis	Difference ratio%
5-storey	1.53	1.25	18.30
10-storey	3.24	2.66	17.9
14-storey	5.06	4.11	18.77
17-storey	8.13	5.4	33.58
20-storey	12.8	6.71	47.58
24-storey	21.4	7.54	64.77
30-storey	41.3	7.74	81.26

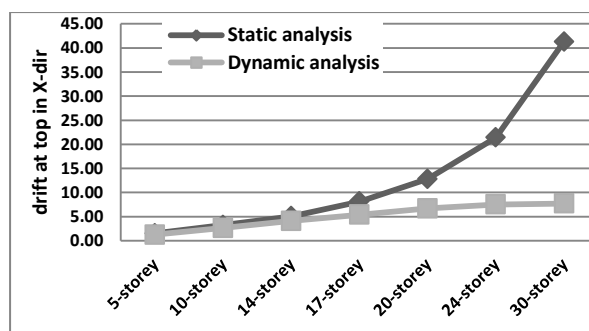
**Table (5):** Drift values for both static and dynamic analysis by UBC 1997

Buildings	Static analysis	Dynamic analysis	Difference ratio%
5-storey	1.51	1.26	16.56
10-storey	3.35	2.57	23.28
14-storey	5.38	4.03	25.09
17-storey	7.24	5.36	25.97
20-storey	9.6	6.67	30.52
24-storey	16.4	8.62	47.44
30-storey	32	12	62.5

Figures (3, 4 and 5) represent the values of displacements at top versus each case for ECP 2012, EC8: 2004 and UBC 1997 respectively



**Figure (3):** Drift values for both static and dynamic analysis according to ECP 2012



**Figure (4):** Drift values for both static and dynamic analysis according to EC8: 2004

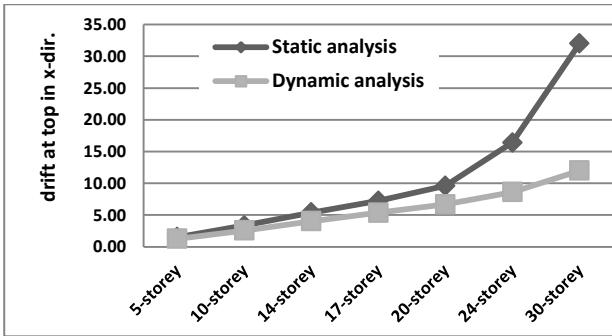


Figure (5): Drift values for both static and dynamic analysis according to UBC 1997

Figure (6) represent the difference ratios between the values of displacement at top for both static and dynamic analysis versus each case and code

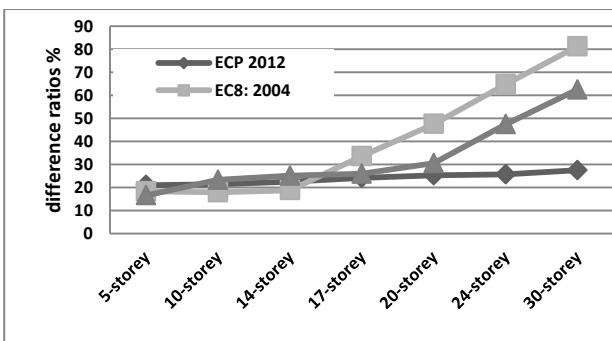


Figure (6): Difference ratio between drifts at top for static and dynamic analyses

**b. Results of Overturning Moments at Base:-**

Tables (6, 7 and 8) give the results of overturning moments at base versus each case for ECP 2012, EC8: 2004 and UBC 1997 respectively

Table (6): BM at base for both static and dynamic analysis for each case by ECP 2012

Buildings	BM at base (t.m × 10 <sup>3</sup> )		Difference ratio%
	Static analysis	Dynamic analysis	
5-storey	3.41	2.76	19.06
10-storey	8.65	7.22	16.532
14-storey	14.4	12.1	15.972
17-storey	22.6	17.9	20.796
20-storey	34.7	25.1	27.666
24-storey	52.8	32.5	38.447
30-storey	92.5	52.7	43.027

Table (7): BM at base for both static and dynamic analysis for each case by EC8: 2004

Buildings	BM at base (t.m × 10 <sup>3</sup> )		Difference ratio%
	Static analysis	Dynamic analysis	
5-storey	7.56	6.08	19.57
10-storey	15.6	12.4	20.513
14-storey	20.7	15.7	24.155
17-storey	29.2	17.9	38.699
20-storey	41.3	20	51.574
24-storey	60.6	19.4	67.987
30-storey	98.2	16.2	83.503

Table (8): BM at base for both static and dynamic analysis for each case by UBC 1997

Buildings	BM at base (t.m × 10 <sup>3</sup> )		Difference ratio%
	Static analysis	Dynamic analysis	
5-storey	7.47	6.13	17.93
10-storey	16	11.8	26.25
14-storey	21.6	15.3	29.167
17-storey	25.4	17.7	30.315
20-storey	29.8	19.7	33.893
24-storey	44.4	22.4	49.55
30-storey	72.6	26	64.187

Figures (7, 8 and 9) represent the values of displacements at top versus each case for ECP 2012, EC8: 2004 and UBC 1997 respectively

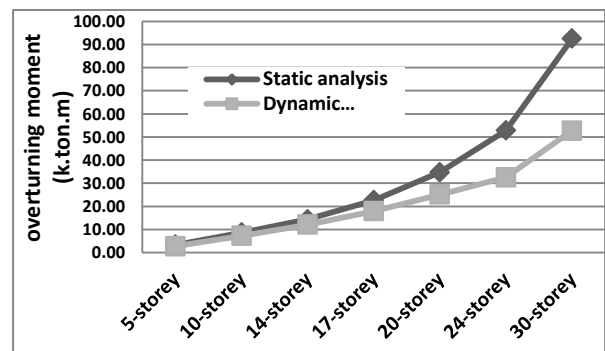


Figure (7): BM at base for both static and dynamic analysis according to ECP 2012

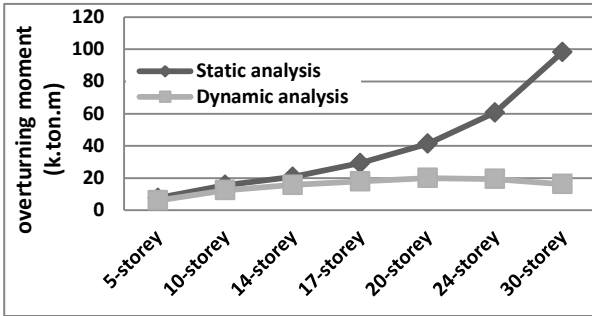


Figure (8): BM at base for both static and dynamic analysis according to EC8: 2004

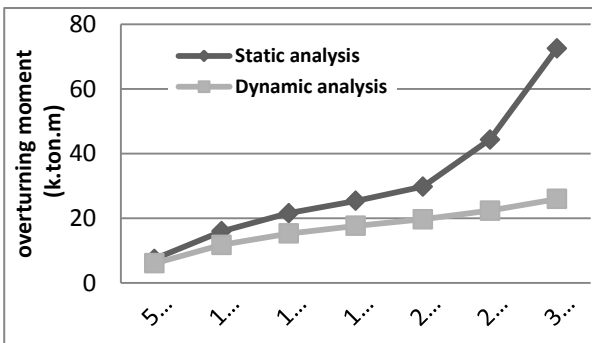


Figure (9): BM at base for both static and dynamic analysis according to UBC 1997

Figure (10) represent the difference ratios between the values of overturning moments at base for both static and dynamic analysis versus each case and code

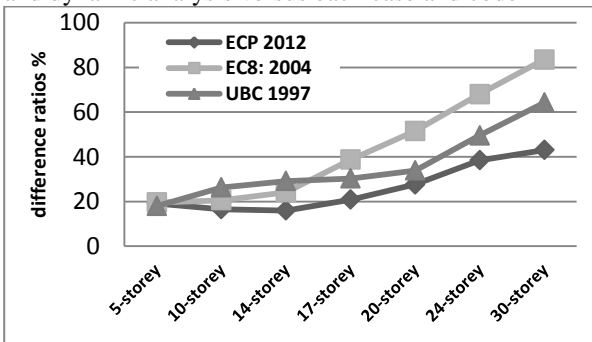


Figure (10): Difference ratio between BM at base for static and dynamic analyses

### Discussion of Results:-

It is seen from the previous figures that the values of both drifts at top and overturning moments obtained by response spectrum analysis and static analysis are closed to each other especially for low-rise buildings. While, static analysis gives higher values for drifts at top and overturning moments rather than the other method of analysis, especially in high levels.

Regarding the results of ECP 2012, Table (3) and Fig. (3) Show that the differences between the results of drift for both static and dynamic are almost

insignificant. On the other hand, Table (6) and Fig. (7) Show that the differences between the results of overturning moment are largely increased especially from the 20-storey building whereas, the difference ratio in the 17-storey building is 20.79% then the percent increased to be 27.66%, 38.44% and 43.02% for the 20, 24 and 30-storey building respectively.

Regarding the results of EC8: 2004, Table (4,7) and Fig. (4,8) Show that the differences between the results in the first three buildings are insignificant in both results relevant to drifts at top and overturning moments at base. On the other hand, the differences between the results in the last four buildings are largely increased with the height. Whereas, the differences ratio in the 14-storey building for drift at top and overturning moments are 15.97% and 24.15% respectively then the ratios of drift at top increased to be 20.8%, 27.66%, 38.44% and 43.02% similarly, the ratios of overturning moments increased to be 38.70%, 51.57%, 67.98% and 83.5% for the last four heights respectively.

Regarding the results of UBC 1997, Table (5,8) and Fig. (5,9) Show that that the differences between the results in the first five buildings are insignificant in both results relevant to drifts at top and overturning moments. On the other hand, the differences between the results in the last two buildings in both drifts at top and overturning moments are largely increased with the height. Whereas, the differences between the results in the 20-storey building for drift at top and overturning moments are 30.52% and 33.89% respectively then the ratios increased to be 47.44% and 62.5% in case of drift at top similarly, the ratios increased to be 49.55% and 64.18% in case of overturning moments for the last four heights respectively.

### Conclusions:-

- 1) The equivalent static method can be used as same as the response spectrum analysis method for seismic analysis of low-rise building however for medium to high-rise building the equivalent static method should not be used because it gives higher values for drifts at top and overturning moments rather than other methods of analysis, especially in higher stories
- 2) In ECP 2012, the equivalent static method may be applied on buildings with less than 60m height. While, In EC8: 2004, the equivalent static method may be applied on buildings less than 40m height. On the other hand, UBC 1997 may permit using it up to 70m height. Thereby using equivalent static method in seismic analysis above these heights will be accompanied by uneconomic values for design

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